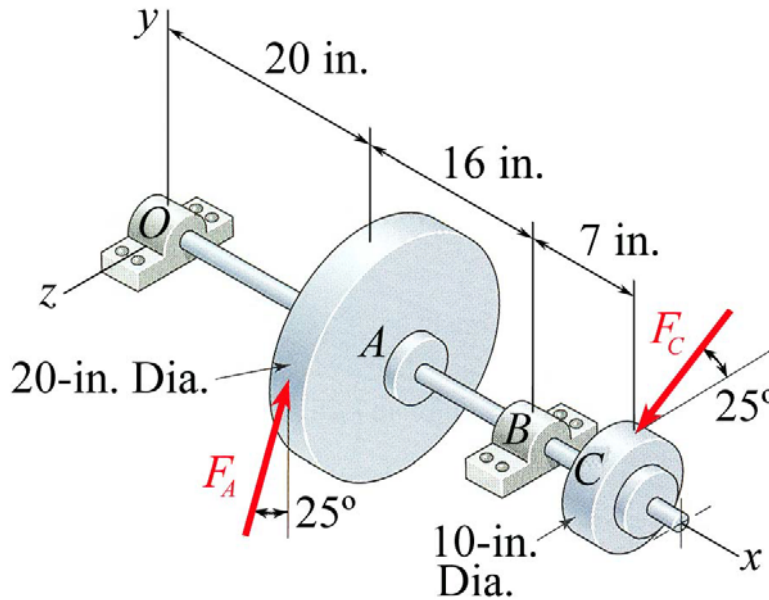


- ④ Derive the octahedral shear stress  $\tau_{oct}$ .
- ⑥ The gear forces shown are parallel to the  $yz$  plane, where  $F_A = 500$  lb, the bearings at  $O$  and  $B$  may be taken as simple supports, and the shaft has  $S_y = 60$  kpsi. For static analysis and a factor of safety of 3.5, use *distortion-energy theory* to find the minimum safe diameter  $d$  of the shaft.



1.

$$[\sigma_{ij}] = \begin{bmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{bmatrix} \quad (\frac{1}{2}) \quad n_i \Rightarrow \frac{1}{\sqrt{3}} \langle 1, 1, 1 \rangle \quad (\frac{1}{2}) \quad t_i = \sigma_{ji} n_j \Rightarrow \frac{1}{\sqrt{3}} \langle \sigma_1, \sigma_2, \sigma_3 \rangle \quad \textcircled{1}$$

$$t^2 = t_i t_i = \frac{1}{3} (\sigma_1^2 + \sigma_2^2 + \sigma_3^2) \quad (\frac{1}{2}) \quad \sigma_{oct} = t_i n_i = \frac{1}{3} (\sigma_1 + \sigma_2 + \sigma_3) \quad (\frac{1}{2})$$

$$\tau_{oct}^2 = t^2 - \sigma_{oct}^2 \quad (\frac{1}{2}) \quad \therefore \tau_{oct} = \frac{1}{3} \left[ (\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \right]^{1/2} \quad (\frac{1}{2})$$

2.  $F_A = 500$  lb Draw FBD  $\textcircled{1}$   $F_C = 1000$  lb  $(\frac{1}{2})$   $\mathbf{O} = -283.5775\mathbf{j} + 270.1417\mathbf{k}$  lb  $\textcircled{1}$   
 (or  $\mathbf{B} = 253.042\mathbf{j} - 965.140\mathbf{k}$  lb)  $M_A = 7833.077$  lb·in.  $(\frac{1}{2})$   $M_B = 7000$  lb·in.  $(\frac{1}{2})$

**At A:**  $\sigma_x = 9973.38 r^{-3}$   $(\frac{1}{2})$   $\tau_{xy} = -2884.87 r^{-3}$   $(\frac{1}{2})$   $\sigma' = 11155.1 r^{-3}$   $(\frac{1}{2})$   $n = 3.5$   
 $S_y = 60 \times 10^3$  psi  $n = S_y / \sigma'$   $r = 0.8666$  in.  $d = 1.733$  in.  $(\frac{1}{2})$  Use  $d = 1.75$  in.  $(\frac{1}{2})$